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## Comparison study of Trilateral Rankine Cycle, Organic Flash Cycle and basic Organic Rankine Cycle for low grade heat recovery

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### Abstract

Organic Rankine Cycle (ORC) has been widely used for the recovery of low-grade heat into power such as solar energy and industrial waste heat. The overall thermal efficiency of ORC is affected by large exergy destruction in the evaporator due to the temperature mismatching between the heat source and working fluid. Trilateral Cycle (TLC) and Organic Flash Cycle (OFC) have been recognized as potential solutions because of their better performance on temperature matching between the heat source and working fluid at the evaporator. In this study, thermodynamic models of above three cycles are established in MATLAB/REFPROP. Results indicate that TLC obtains the largest net power output, thermal efficiency and exergy efficiency of 13.6 kW, 14.8% and 40.8% respectively at the evaporation temperature of 152°C, which is 37% higher than that of BORG (9.9 kW) and 58% higher than that of OFC (8.6 kW). BORG is more suitable under the conditions low evaporation temperature is relatively low due to the achieved maximum net power output, thermal efficiency and exergy efficiency. OFC has the minimum net power output, thermal efficiency and exergy efficiency under all the conditions of evaporation temperature compared to TLC and BORG. As for the  $UA$  value, TLC has the largest one ranging from 7.9 kW/°C to 8.8 kW/°C under all conditions while OFC gains the minimum  $UA$  value at low evaporation temperature and BORG gains the minimum  $UA$  value at high evaporation temperature.

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**Keywords:** Trilateral Rankine Cycle; Organic Flash Cycle; thermodynamic performance; total heat transfer coefficient

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**1. Introduction**

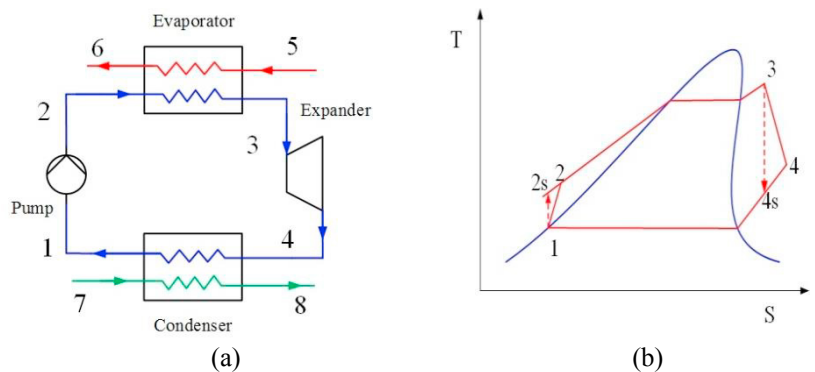
The growth of population and economic development causes escalating energy consumption and many other environmental problems by burning fossil fuels [1, 2]. The utilization of low grade heat energy can potential reduce the demand of conventional energy sources and improve the overall efficiency of the existing energy systems [3, 4]. ORCs are considered as a practical solution because of their simplicity, reliability, and flexibility [5-7]. Many researches have been conducted to study the performance of ORC for waste heat recovery [8-11]. However, one of the main problems in ORC based power plants is the high exergy destruction in these cycles. The main source of exergy destruction in ORC is evaporator because of the temperature mismatching between the source and the working fluid [1, 12, 13].

Among the proposed novel cycles, Trilateral Cycle (TLC) is one of the most promising alternatives among the heat recovery-to-power technologies, due to its higher heat transfer efficient from heat source to working fluid, compact system configuration, high performance at relatively low compression work and low-to-moderate expander inlet temperature [14, 15]. For TLCs there are some transformations and organic flash cycle (OFC) is one of the most important system, which can potentially replace the two-phase expander required in TLC and therefore reduce the capital cost of the system [16, 17]. Compared with basic ORCs, which has been widely adopted in the existing power plants, the TLC and OFC are still in a state of technical development. In this paper, the net work power, energy efficiency, exergy efficiency and total heat transfer coefficient of TLC, OFC and ORC have been investigated and compared in order to identify the differences of these systems for various application conditions.

**2. System description**

*2.1. Description of BORC*

The schematic and T-S diagram of BORC system are depicted in figure 1. The BORC system consists of an evaporator, a condenser, a pump and an expander. In state 1 the working fluid is saturated liquid with temperature  $T_1$  and pressure  $p_1$ . Then the pressure of the working fluid is elevated to  $p_2$  by the pump



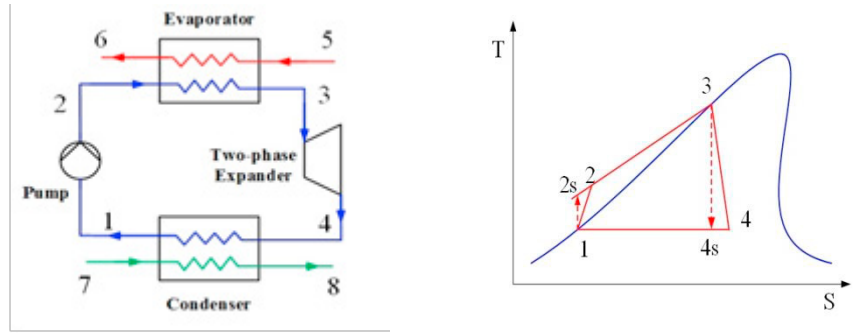
**Fig. 1.** Basic Organic Rankine cycle  
(a) Schematic diagram; (b) T-s diagram

with the isentropic pump efficiency  $\eta_{sp}=(h_{2s}-h_1)/(h_2-h_1)$ , which is the maximum pressure in the cycle. After that, the liquid is heated to the temperature  $T_3$  in an isobaric process, which is the maximum temperature in the cycle. However it is lower than the critical temperature. The isobaric heating process includes heating of liquid to the saturated state, evaporation of the liquid and finally superheating of the vapor. At state 3 the overheated vapor enters the turbine and expands to the pressure  $p_4$  at state 4 with isotropic expander efficiency  $\eta_{se}=(h_4-h_3)/(h_{4s}-h_3)$  and work is delivered in this process. Eventually, from state 4 the vapor is first precooled to the saturated state with temperature  $T_1$  and then is condensed to state 1 in an isobaric process.

*2.2. Description of TLC*

The schematic and T-S diagram of TLC system are depicted in figure 2. The TLC system consists of a heat exchanger, a condenser, a pump and a two-phase expander. In state 1 the working fluid is saturated liquid with temperature  $T_1$  at the vapor pressure  $p_1$ . Then the liquid pressure is increased to  $p_2$  by the pump at state 2 in the homogeneous liquid. Thereafter, the working liquid enters the heat exchanger where it is heated to the boiling point

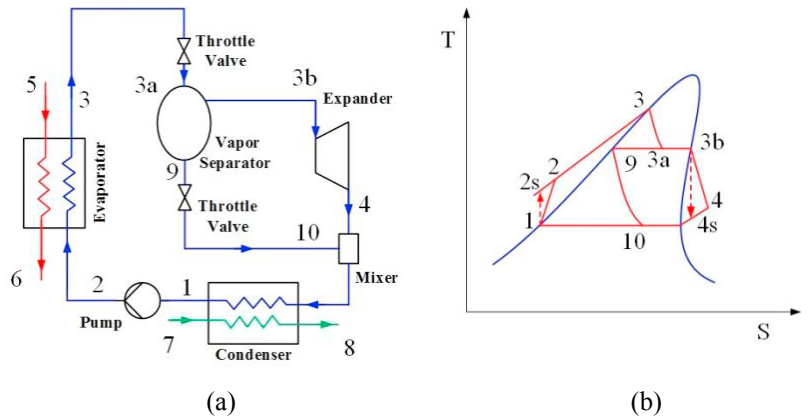
at pressure  $p_2$ , which is state 3. The temperature  $T_3$  is the boiling temperature at pressure  $p_2$ . Starting from state 3, the working fluid directly enters the two-phase expander. In the two-phase expander the working liquid expands into the wet vapor region and gradually reaches the state 4 with the pressure  $p_1$  and temperature  $T_1$ . At state 4 the vapor content is  $x$ . during the liquid expanding process work is delivered. Eventually, the wet vapor is completely condensed till it reaches state 1.



(a) (b)  
**Fig. 2.** Trilateral Rankine Cycle  
 (a) Schematic diagram; (b)  $T$ - $s$  diagram

2.3. Description of OFC

System layout and  $T$ - $s$  diagram of an OFC are presented in Fig. 3(a) and (b) respectively. Compared to TLC system, in the OFC the saturated working fluid at state 3 is throttled to the expander inlet pressure with isenthalpic process and allowed to enter the vapor separator instead of entering the expander directly. Saturated vapor flowing out the vapor separator expands (from state 3b to 4) in the expander to produce work. Exhausted vapor coming out from expander (state 4) mixes with liquid coming out of throttle (state 9 to 10). Then the total mass of working fluid is condensed to saturated liquid at condenser pressure at the condenser.



(a) (b)  
**Fig. 3.** Organic Flash Cycle  
 (a) Schematic diagram; (b)  $T$ - $s$  diagram

3. Thermodynamic models of the systems

3.1. Thermodynamic model for BORC

For a given mass flow rate of source  $m_h$ , the mass flow rates of working fluid  $m_w$  and  $m_c$  can be determined from the energy balances in the heat exchangers as Eq. (1) and (2), where  $m$  is the mass flow rate,  $T$  is the temperature,  $h$  is the specific enthalpy, and  $c_p$  is the isobaric specific heat.

The rate of the heat received by the evaporator  $Q_{in}$ , heat

$$m_w = c_{p,h} m_h (T_5 - T_6) / (h_2 - h_3) \tag{1}$$

$$m_w = c_{p,c} m_c (T_8 - T_7) / (h_1 - h_4) \tag{2}$$

$$Q_{in} = m_w (h_2 - h_3) = c_{p,h} m_h (T_5 - T_6) \tag{3}$$

$$Q_{out} = m_w (T_4 - T_1) = c_{p,c} m_c (T_8 - T_7) \tag{4}$$

$$W_e = m_w (h_3 - h_4) \tag{5}$$

$$W_p = m_w (h_2 - h_1) \tag{6}$$

$$W_{net} = W_e - W_p \tag{7}$$

$$\eta_{th} = W_{net} / Q_{in} \tag{8}$$

$$E_{total} = m_w [(h_{in} - h_0) - T_0 (S_{in} - S_0)] \tag{9}$$

$$\eta_{ex} = W_{net} / E_{total} \tag{10}$$

$$UA = \Delta Q / \Delta T_{lm} \tag{11}$$

$$\Delta T_{lm} = (\Delta T_1 - \Delta T_2) / \ln(\Delta T_1 / \Delta T_2) \tag{12}$$

dissipation at condenser  $Q_{out}$ , power output from expander  $W_e$ , pumping power consumption of the pump  $W_p$ , net power output of the cycle  $W_{net}$ , thermal efficiency  $\eta_{th}$ , total exergy loss  $E_{total}$  and exergy efficiency  $\eta_{ex}$  can be evaluated as Eq. (3)-(7).

The UA (total heat transfer coefficient) value of heat exchangers has been calculated in this study and the calculation method can be defined as Eq. (11), where  $\Delta Q$  denotes the heat flux of a heat exchanger.  $\Delta T_{lm}$  denotes the log-mean temperature difference, which can be calculated by log-mean temperature difference method (LMTD) presented in Eq. (12).

$$W_p = m_w h_3 - m_w [x_1 \cdot h_4'' + (1 - x_1) \cdot h_4'] \tag{13}$$

3.2. Thermodynamic model for TLC

$$x_2 = (h_{3b} - h_{3a}) / (h_3 - h_{3a}) \tag{14}$$

The characters of TLC are steps from state 1 to 2 and from state 3 to 4. From state 1 to 2, the liquid is heated to saturated liquid which can be calculated by Eq. (3). Due to the two-phase expander, working liquid at outlet of expander is wet vapor with vapor mass fraction of  $x_1$ . The energy conservation equation is defined as Eq. (13)

3.3. Thermodynamic model for OFC

The throttle process from state 3 to 4 determines the mass fraction of vapor  $x_2$  entering the expander. Due to the isenthalpic process, the  $x_2$  can be calculated by equation (14). Other process can be calculated by equation (1) to (12).

**Table 1.** Initial parameters

Parameters	Value
Inlet temperature of heat source (K)	473
Mass flow rate of heat source (kg/s)	1
Condense temperature (K)	315
Inlet temperature of coolant (K)	298

**4. Results and discussion**

Working fluid is *R245fa* and calculation is based on the same initial conditions for the three cycles. Some initial parameters are listed in Table 1. Net power output, thermal efficiency, exergy efficiency, UA value and total waste heat are evaluated with different evaporation temperature of working fluid. The corresponding results are shown in Fig. 4.

4.1 Evaluation of net power output

Fig. 4(a) shows the net power output increases with the rise of evaporation temperature. OFC has the lowest net power output ranging from 0.6 kW to 8.6 kW at all the operating condition compared to BORG and TLC. The net power output of TLC is first lower than that of BORG with the increasing of evaporation temperature, however, the difference keeps decreasing. When evaporation temperature is beyond 125 °C net power output of TLC is larger than that of BORG. The maximum net power output of TLC (13.6 kW) is 37% higher than that of BORG (9.9 kW) and 58% higher than that of OFC. The results illustrates TLC is more suitable for the waste heat recovery under high evaporation temperature while BORG is well matched to the lower evaporation temperature.

4.2 Evaluation of thermal efficiency

Fig. 4(b) shows the comparison of system thermal efficiency for the three cycles. Thermal efficiency of three cycles improves with the increase of evaporation temperature. The change of thermal efficiency is consistent with the net power output. Thermal efficiency of OFC is lowest ranging from 0.6% to 9.4% under all the operating conditions. Thermal efficiency of TLC is first lower than that of BORG with the rise of evaporation temperature, then it becomes larger than that of BORG when the evaporation temperature exceeds 130 °C. The maximum thermal efficiency of TLC is 14.8% at the evaporation temperature of 153 °C, which is 40% higher than that of

BORC (10.6%) and 57% higher than that of OFC. The results illustrates TLC is more efficient for the waste heat recovery under high evaporation temperature while BORC have better performance at the lower evaporation temperature.

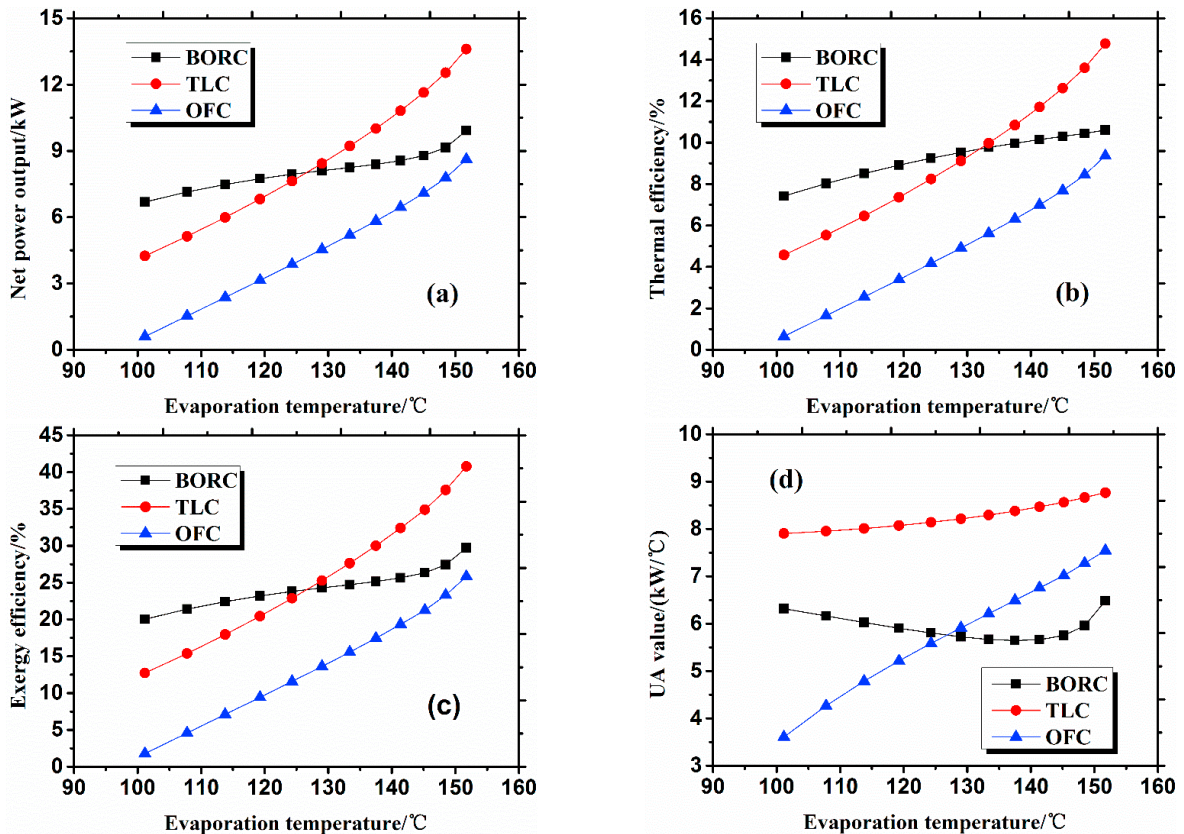


Fig. 4 (a) net power output; (b) thermal efficiency; (c) exergy efficiency; (d)  $UA$  value

#### 4.3 Evaluation of exergy efficiency

Similarly, it is observed from Fig. 4(c) exergy efficiency of three cycles keep improving with the rise of evaporation temperature. Exergy efficiency of OFC is lowest ranging from 1.8% to 25.8% under all the operating conditions. Exergy efficiency of TLC is first smaller than that of BORC with the rise of evaporation temperature, then it expands dramatically and when the evaporation temperature exceeds 128 °C it is larger than that of BORC. The exergy efficiency of TLC ranges from 12.7% to 40.8%, indicating the superior property of matching to the heat source. The maximum exergy efficiency of TLC is 37% larger than that of BORC, while the maximum exergy efficiency of BORC is 29.7% and it is 58% larger than that of OFC. Based on the analysis above, it can be concluded TLC is more suitable for conditions with high evaporation temperature while for BORC larger exergy efficiency is achieved at low evaporation in the present study.

#### 4.4 Evaluation of $UA$ value

The smaller  $UA$  value means the more economical of the ORC system. It is observed from Fig. 4(d) that the  $UA$  value of TLC keeps increasing with the rise of evaporation (ranging from 7.9 kW/°C to 8.8 kW/°C) and it is largest

at all the operating conditions. The  $UA$  value of BORC first decreases with the rise of evaporation temperature and reaches the minimum value of  $5.7 \text{ kW}/^\circ\text{C}$  at the evaporation temperature of  $138^\circ\text{C}$ , then it gradually increases with the rise of evaporation temperature and attains the maximum value of  $6.5 \text{ kW}/^\circ\text{C}$  eventually. For the OFC, the  $UA$  value rising substantially with the increase of evaporation temperature and ranges from  $3.6 \text{ kW}/^\circ\text{C}$  to  $7.5 \text{ kW}/^\circ\text{C}$ . Comparing the three cycles, OFC has lower  $UA$  value at lower evaporation temperature (not beyond  $128^\circ\text{C}$ ) and BORC has better economic system performance at higher evaporation temperature (beyond  $128^\circ\text{C}$ ).

## 5. Conclusions

In the present study, comparative thermodynamic as well as economic analyses under different evaporation temperature are performed for BORC, TLC and OFC while producing power utilizing low grade waste heat of a free flue gas. Conclusions drawn from this study are

1. Net power output increases with the rise of evaporation temperature. OFC has the minimum net power output at all the operating conditions. When the evaporation temperature is higher than  $125^\circ\text{C}$ , TLC obtains the maximum net power output  $13.6 \text{ kW}$ , which is  $37\%$  higher than that of BORC ( $9.9 \text{ kW}$ ) and  $58\%$  higher than that of OFC ( $8.6 \text{ kW}$ ).

2. Thermal efficiency has a similar trend to that of net power efficiency for the three cycles. The comparison of thermal efficiency indicates that OFC has the poorest thermal efficiency at all the operating conditions while TLC achieves the best one of  $14.8\%$ , which is  $40\%$  higher than that of BORC ( $10.6\%$ ) and  $57\%$  higher than that of OFC.

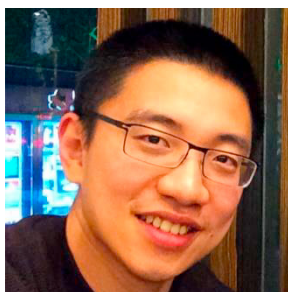
3. Exergy efficiency changes consistently with net power output and thermal efficiency. Analysis of exergy efficiency illustrates that OFC has the lowest exergy efficiency at all the operating conditions. Exergy efficiency of TLC is larger than BORC when the evaporation temperature exceeds  $128^\circ\text{C}$  and it gains the largest value of  $40.8\%$ , which is  $37\%$  larger than that of BORC ( $29.7\%$ ) and  $58\%$  larger than that of OFC.

4. The  $UA$  value of TLC (ranging from  $7.9 \text{ kW}/^\circ\text{C}$  to  $8.8 \text{ kW}/^\circ\text{C}$ ) is largest at all the operating conditions. When the evaporation temperature is beyond  $128^\circ\text{C}$ , the  $UA$  value of BORC is smallest and it reaches the minimum value of  $5.7 \text{ kW}/^\circ\text{C}$  at the evaporation temperature of  $138^\circ\text{C}$ . When the evaporation temperature is lower than  $128^\circ\text{C}$ , OFC obtain the smallest  $UA$  value among three cycles.

5. Considering net power, thermal efficiency, exergy efficiency and  $UA$  value, TLC has better thermodynamic performance but poor economical overall system performance when the evaporation temperature is beyond  $135^\circ\text{C}$ . Reversely, OFC is more economic to be used but the thermodynamic performance is lower than other two cycles.

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### Biography

Dr Yiji Lu, born in June 1989, is currently a research associate in Newcastle University. He graduated from Shanghai Jiao Tong University in 2011 for his bachelor degree, he conducted his M.Phil. and Ph.D. in Newcastle University in 2012 and 2016. His Ph.D. program was fully sponsored by EPSRC and was awarded the ‘2015 Chinese Government Award for Outstanding Self-financed Students Abroad’ from China Scholarship Council. His research interests include but not limited to advanced waste heat recovery technologies, engine thermal management, advanced engine development, engine emission technologies, chemisorption cycles and expansion machines for power generation system. He has been regularly invited to review the manuscripts for the scientific journals including Applied Energy, Applied Thermal Engineering, Energy (the International Journal), and Energy for Sustainable Development.

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