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# Co-optimization of sponge-core bioreactors for removing total nitrogen and antibiotic resistance genes from domestic wastewater

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31 **ABSTRACT**

32 Inadequate sanitation can lead to the spread of infectious diseases and antimicrobial  
33 resistance (AMR) via contaminated water. Unfortunately, wastewater treatment is not  
34 universal in many developing and emerging countries, especially in rural and peri-urban  
35 locations that are remote from central sewers. As such, small-scale, more sustainable  
36 treatment options are needed, such as aerobic-Denitrifying Downflow Hanging Sponge  
37 (DDHS) bioreactors. In this study, DDHS reactors were assessed for such applications,  
38 and achieved over 79% and 84% removal of Chemical Oxygen Demand and  
39 Ammonium, respectively, and up to 71% removal of Total Nitrogen (TN) from  
40 domestic wastes. Elevated TN removals were achieved via bypassing a fraction of raw  
41 wastewater around the top layer of the DDHS system to promote denitrification.  
42 However, it was not known how this bypass impacts AMR gene (ARG) and mobile  
43 genetic element (MGE) levels in treated effluents. High-throughput qPCR was used to  
44 quantify ARG and MGE levels in DDHS bioreactors as a function of percent bypass (0,  
45 10, 20 and 30% by volume). All systems obtained over 90% ARG reductions, although  
46 effluent ARG and TN levels differed among bypass regimes, with co-optimal reductions  
47 occurring at ~20% bypass. ARG removal paralleled bacterial removal rate, although  
48 effluent bacteria tended to have greater genetic plasticity based on higher apparent MGE  
49 levels per cell. Overall, TN removal increased and ARG removal decreased with  
50 increasing bypass, therefore co-optimization is needed in each DDHS application to  
51 achieve locally targeted TN and AMR effluent levels.

52

53 **Keywords:** Antibiotic resistance genes; sustainable wastewater treatment; wastewater  
54 bypass; denitrification; high-throughput qPCR

55

## 56 **1. Introduction**

57 Effective wastewater treatment and community sanitation are critical to global health  
58 and environmental protection. However, almost 2.5 billion people live without access to  
59 even basic sanitation (United Nations, 2015), which impacts infectious disease mortality  
60 and increases exposure to environmental antimicrobial resistance (AMR) via  
61 contaminated water (Hu et al., 2008; Manaia et al., 2016; Pruden et al., 2013; Quintela-  
62 Baluja et al., 2015; WHO, 2014; Zhang et al., 2009a). The impact of water- and waste-  
63 borne AMR releases is most profound in emerging and developing countries because  
64 waste management is not proceeding as rapidly as urbanisation, leading to declining  
65 environmental quality as development occurs. Accordingly, the United Nations has  
66 committed to reduce the lack of sanitation in half by 2030 (United Nations, 2016) and is  
67 espousing the One Health approach to combat AMR in the environment (Robinson et  
68 al., 2016; Singh, 2017). However, problems exist in expanding peri-urban environments  
69 because such locations often lack centralised sewage collection. As such, smaller, local-  
70 scale treatment options are needed to increase wastewater treatment coverage, although  
71 few reliable “small” technologies exist that reduce carbon (C) and total nitrogen (TN)  
72 levels as well as mitigate against waterborne pathogens and AMR releases.

73

74 Denitrifying Downflow Hanging Sponge (DDHS) reactors are a low cost and low  
75 maintenance wastewater treatment option that is suitable for smaller or decentralised  
76 applications (Bundy et al., 2017). DDHS systems can achieve high Chemical Oxygen  
77 Demand (COD), Ammonium-Nitrogen ( $\text{NH}_4\text{-N}$ ) and TN removals by using bipartite  
78 aerobic-anoxic sponge layers and a raw wastewater bypass to supply extra carbon to  
79 lower submerged layers to promote denitrification (Isaacs & Henze, 1995; Schipper et  
80 al., 2010). The wastewater bypass is crucial to DDHS systems because, when carbon is

81 removed in top aerobic layers, lower layers become C-limited for denitrification,  
82 restricting conversion of nitrate to N<sub>2</sub>, which is critical for application in places like  
83 China with tight TN discharge standards (Ministry of Environmental Protection (MEP),  
84 2002). Further, DDHS systems use minimal energy because they employ passive  
85 aeration and also provide design flexibility in the sponge core (e.g. varying redox zones,  
86 reactor volumes and density ratios) that can be customised to local conditions. However,  
87 little is known about how DDHS reactors remove AMR genes (ARGs) and mobile  
88 genetic elements (MGEs) during treatment. There is reason to believe DDHS systems  
89 may be quite effective because sequenced redox conditions can enhance ARG removal  
90 (Christgen et al., 2015).

91

92 Here we used high-throughput qPCR (HTH-qPCR) to compare influent and effluent  
93 ARGs and MGEs in DDHS bioreactors as a function of wastewater bypass. Selected  
94 microbial culturing also was performed for Gram (-) Extended Spectrum Beta-  
95 Lactamase-producing bacteria (ESBL-producing) to compliment ARG and MGE data as  
96 well as TN and other treatment metrics. Such data is key for process optimisation,  
97 especially where TN and AMR reductions are both desired, such as places where  
98 improved decentralised treatment is urgently needed (e.g. China, India).

99

## 100 **2. Material and Methods**

101

### 102 **2.1. DDHS reactor configurations**

103 Four bench-scale DDHS bioreactors were set up as previously described (Bundy et al.,  
104 2017) and operated in parallel for 210 days. Each continuous-flow bioreactor was  
105 identical, made from PVC cylinders (0.5 m tall x 0.14 m internal diameter; working  
106 volumes = 3 L), and configured to include internal recirculation and a wastewater

107 bypass (also called “shunting”) to the submerged layer (Figure S1; see Supporting  
108 Information, SI). DDHS reactor cores consist of an upper hanging sponge layer exposed  
109 to air from above, below, and through side vents, which provide passive aeration for C-  
110 removal and nitrification; and a bottom anoxic sponge layer for denitrification,  
111 prospectively enhanced by wastewater shunting. Reactors were seeded with nitrifying  
112 return activated sludge (RAS) to encourage biofilm growth within the sponge matrix,  
113 and were operated in continuous-flow mode with an organic loading rate of 0.4 kg  
114 COD/m<sup>3</sup>-sponge/day (HRT = 0.6 days) and under room temperature environment (22-  
115 23 °C) (Bundy et al., 2017).

116

117 The reactors were designated R-S0, R-S10, R-S20 and R-S30, being defined by  
118 different bypass percentages; 0%, 10%, 20% and 30% (% of total wastewater by  
119 volume), respectively. R-S0 with no bypass was the control unit. Previous work showed  
120 TN removals were most efficient at bypass levels of 20 to 30% (Bundy et al., 2017). A  
121 10% bypass was included to allow step-wise analysis from zero to 30%, to co-optimize  
122 the DDHS reactor for simultaneous TN and ARG removal.

123

## 124 **2.2. Influent source, routine sample analysis and monitoring**

125 Influent and effluent samples were collected and analysed to monitor treatment  
126 performance. Fresh settled wastewater (post primary settling; called ‘raw’ here) was  
127 collected weekly from a municipal wastewater treatment plant in northern England and  
128 stored at 4 °C prior to use as reactor influent. Raw wastewater was fed in parallel via  
129 influent pumps to all reactors from an 18-L carboy retained in a fridge located next to  
130 the reactors. Analyses on influent and effluents included Soluble COD (COD<sub>s</sub>), Total  
131 COD (COD<sub>t</sub>), Total Suspended Solids (TSS), Volatile Suspended Solids (VSS), Total

132 Kjeldahl Nitrogen (TKN), Ammonium-Nitrogen (NH<sub>4</sub>-N), Nitrite (NO<sub>2</sub>-N) and Nitrate  
133 (NO<sub>3</sub>-N), as previously described (Bundy et al., 2017). Mean wastewater and effluent  
134 characteristics are summarised in Table S1 (see SI).

135

### 136 **2.3. Sample collection, DNA extraction and ARB enumeration**

137 Sample collection for ARG, MGE, and antibiotic resistant bacteria (ARB; i.e., ESBL-  
138 producing isolates) quantification was conducted during quasi-steady-state conditions  
139 (based on C and TN removal data) during three biweekly sampling regimes. Altogether,  
140 15 samples were collected for AMR-related analyses, consisting of five samples per  
141 sampling week: one influent from parallel feeding points and four DDHS final effluents  
142 from the respective final discharge points.

143

144 For ARG and MGE quantification, samples were collected and concentrated to obtain  
145 adequate biomass for DNA extraction. Effluent samples were collected, stored on ice  
146 (for 2 to 4 hours), and then filtered through 0.20 µm pore-sized Polyethersulfone filters  
147 (Pall Corporation, USA) to harvest the cells, whereas influent samples were collected  
148 and concentrated by centrifugation at 4000 x g for 10 minutes (Scientific laboratory,  
149 UK). Filtrates and centrates were discarded, respectively, and filter paper and pellets  
150 were stored at -20°C prior to subsequent DNA extraction, using the FastDNA SPIN Kit  
151 for Soil and a FastPrep-24 Homogeniser (MP Biomedicals, Santa Ana, CA, USA).  
152 Following extraction, DNA samples were checked for purity using a NanoDrop 1000  
153 Spectrophotometer (Thermo Scientific, UK) and DNA concentrations were quantified  
154 by using the Qubit 2.0 Fluorometer (Invitrogen, UK). DNA samples were stored at -  
155 80°C prior to downstream analysis.

156

157 In parallel, influent and effluent samples were screened for ESBL-producing  
158 *Enterobacteriaceae*, using ChromID ESBL selective chromogenic media (Biomérieux,  
159 UK). Raw wastewater samples were serially diluted in 1 x sterile phosphate buffer  
160 saline (PBS) solution and 100- $\mu$ L aliquots were plated in triplicate per dilution per  
161 sample. Viable ESBL-producing *E. coli* and *KESC* isolates (i.e., *Klebsiella*,  
162 *Enterobacter*, *Serratia*, *Citrobacter*) were counted after 24 hours of incubation at 37°C  
163 and reported as CFUs/100 mL.

164

#### 165 **2.4. High-throughput quantitative PCR (HTH-qPCR)**

166 Abundance and diversity of ARGs and MGEs were quantified by HTH-qPCR using the  
167 SmartChip Real-time PCR (Warfergen Inc. USA) (Su et al., 2015). A total of 296  
168 primer sets (Table S2) were used to screen for ARGs and MGEs, including 293  
169 validated primer sets targeting 284 ARGs, representing potential resistance to nine  
170 major classes of antibiotics. Eight transposase genes, two integron-associated genes  
171 (universal class I integron-integrase gene, *intI*; and the clinical class 1 integron-integrase  
172 gene, *cintI*); and one eubacterial 16S rRNA gene are also included. Target genes were  
173 originally identified with BLAST on the Antibiotic Resistance Genes Database (ARDB)  
174 or the National Center for Biotechnology Information (NCBI) database.

175

176 HTH-qPCR amplification was conducted as follows: 100- $\mu$ L reaction containing (final  
177 concentration) 1  $\times$  LightCycler 480 SYBR® Green I Master Mix (Roche Inc., USA),  
178 nuclease-free PCR-grade water, 1 ng/ $\mu$ L BSA, 9 ng/ $\mu$ L DNA template, and 1  $\mu$ M of  
179 each forward and reverse primer. The thermal cycle was as follows: initial denaturation  
180 at 95 °C for 10 min, followed by 40 cycles of denaturation at 95 °C for 30 s, annealing  
181 at 60 °C for 30 s, and finally with a melting curve analysis auto-generated by the

182 programme. Corroborating 16S rRNA quantification targeting universal eubacteria for  
183 the same samples was performed using conventional qPCR. Standard curves and the  
184 same 16S rRNA primer sequences were used to quantify 16S gene copies for sample  
185 normalisation (Looft et al., 2012; Ouyang et al., 2015).

186

## 187 **2.5. Genomic data screening and analysis**

188 Raw HTH-qPCR data was cleaned using SmartChip qPCR Software (V 2.7.0.1), which  
189 removes data from wells with multiple melting peaks or inefficient amplification (i.e.,  
190 outside 90% to 110%). Cleaned data from three independent samples (one per week per  
191 sampling location) were then screened according to their threshold cycle value ( $C_T$ ).  
192 Samples with a  $C_T > 31$  were removed, which previous experience suggested are  
193 probable false positives (i.e.,  $C_T = 31$  was the detection limit).

194

195 Normalised gene copy numbers of ARGs and MGEs were calculated as described in  
196 previous studies (Chen et al., 2016; Ouyang et al., 2015). Bacterial cell numbers were  
197 estimated by dividing quantified 16S rRNA copy numbers by the average number of  
198 16S rRNA per bacterium (estimated at 4.1 based on the Ribosomal RNA Operon Copy  
199 Number Database, rrnDB version 4.3.3) (Klappenbach et al., 2001).

200

201 One-way analysis of variance (ANOVA) tests were performed on the three biweekly  
202 ARG datasets and metadata, and statistical comparisons confirmed no significant  
203 variations existed among biweekly sampling events (i.e.  $p > 0.05$ ). ARG and MGE  
204 levels from the three biweekly datasets were used for subsequent comparisons among  
205 influent and reactors effluents.

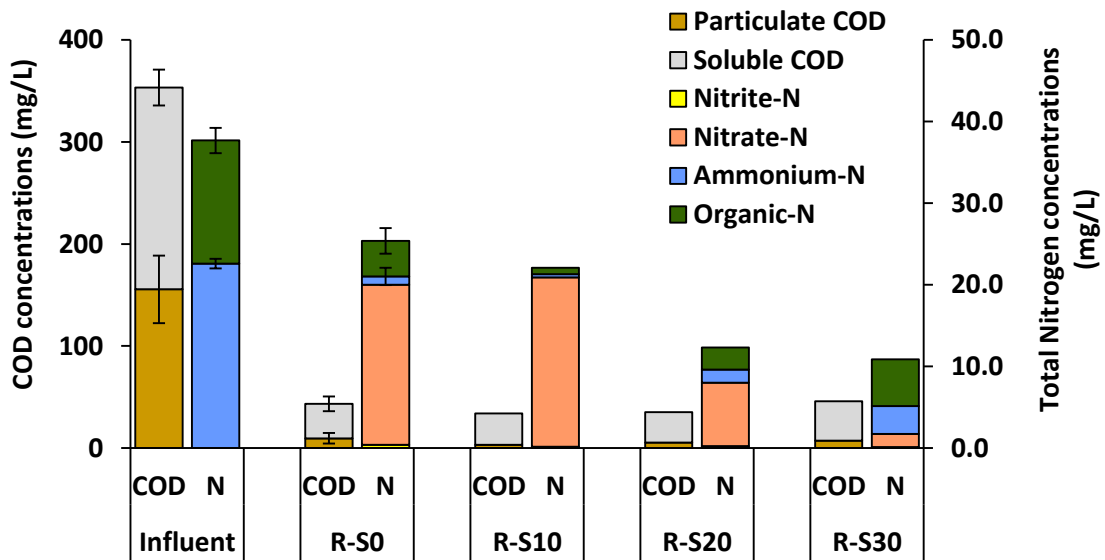
206



207 **3. Results and discussion**

208 **3.1. Enhanced denitrification for decentralised wastewater treatment**

209 Reactor performance data of the DDHS units is shown in Figure 1 and shows  
 210 differences among bypass schemes. COD<sub>s</sub> and COD<sub>t</sub> removal efficiencies always were  
 211 over 79% and 83%, respectively, and NH<sub>4</sub>-N and solids (TSS and VSS; see Table S1)  
 212 removals were consistently over 84% and 90%, respectively. Despite the addition of  
 213 bypass wastewater in R-S10, R-S20 and R-S30, COD removal efficiencies did not  
 214 significantly differ versus bypass levels ( $p > 0.05$ ). However, TN removal rates  
 215 improved dramatically with increasing bypass with significantly lower effluent NO<sub>3</sub>-N  
 216 levels in higher bypass units (see Table S1, paired t-test;  $p < 0.001$ ). Gross TN%  
 217 removals were 28.5%, 37.6%, 64.5% and 71.0% for R-S0, R-S10, R-S20 and R-S30,  
 218 respectively, indicating wastewater bypass does enhance denitrification. Greater COD  
 219 reductions in R-S20 and R-S30, and lower effluent NO<sub>3</sub>-N levels (presumed converted  
 220 to N<sub>2</sub>) suggest increased denitrification is occurring as designed (Bundy et al., 2017).



221

222 **Figure 1.** DDHS reactors mean performance as a function of wastewater bypass.  
223 Stacked bars present mean COD levels (particulate and soluble fractions) and nitrogen  
224 constituents (Ammonium; Nitrate; Nitrite; and Organic-N) in raw wastewater and the  
225 reactor effluents (n = 12 per reactor). Error bars show standard deviation around the  
226 mean; R-S10, R-S20 and R-S30 had minor standard errors.

227

## 228 **3.2. Abundances and patterns of ARGs and MGEs**

### 229 **3.2.1. Total abundances**

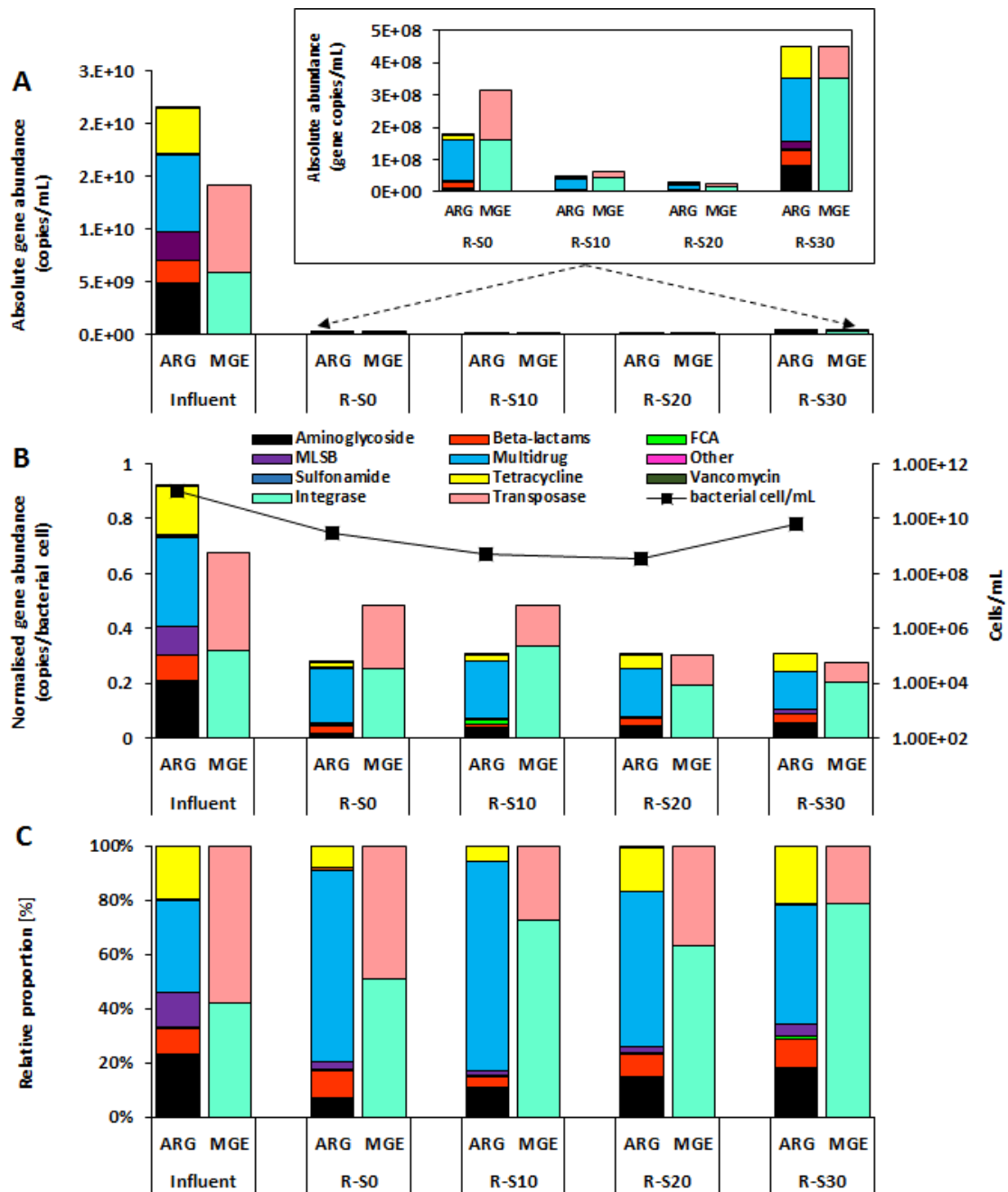
230 HTH-qPCR quantifies both ARGs and MGEs, including ARGs associated with nine  
231 different antibiotic classes, different resistance mechanisms (deactivation, protection,  
232 efflux pump, and unknown), and two MGE groups (transposases and integrons). A total  
233 of 59 unique ARGs ( $2.2 \times 10^{10} \pm 3.7 \times 10^9$  copies/mL) and seven MGEs ( $1.4 \times 10^{10} \pm$   
234  $2.2 \times 10^9$  copies/mL) were detected in influent samples as shown in Figure 2, with  
235 “multidrug” ARGs being most abundant (MDR; 33.8%), followed by aminoglycoside  
236 (23.2%), tetracycline (19.6%), Macrolide-Lincosamide-Streptogramin B (MLSB;  
237 12.9%) and  $\beta$ -lactam (9.5%). Detected influent MGEs were 58% and 42% for  
238 transposase and integrase genes, respectively. [DNA was extracted from biomass](#)  
239 [concentrated from samples by filtering through 0.2um membrane filters, therefore ARG](#)  
240 [levels reported here are cell-associated. Extra-cellular ARGs were not included in this](#)  
241 [study.](#)

242 Absolute ARG abundances significantly declined in all DDHS reactors (see Figure 2A),  
243 consistently achieving 1.0 to 2.0 log reductions (influent vs effluent paired test;  $p <$   
244  $0.05$ ). Effluent ARG levels ranged from  $2.5 \times 10^7$  to  $4.5 \times 10^8$  ARG copies/mL. Highest  
245 absolute ARG removals were seen in the reactors with 10 and 20% bypass as compared  
246 with no bypass (R-S0) and 30% bypass (R-S30). R-S30 had the highest effluent ARG  
247 levels, suggesting “excess” bypass negatively impacts ARG removal. MGE levels also

248 significantly declined in all reactors following similar patterns as for ARGs (Figure 2A).  
249 Overall, the wastewater bypass improves TN removal and achieves efficient ARG  
250 removal, which is co-optimized at ~20% bypass. Highest TN removals were seen at a  
251 30% bypass, but Figure 2 shows ARG removal rates decline, presumably because more  
252 raw wastewater bypasses the aerobic layer, suggesting the aerobic layer may be  
253 particularly important to ARG removal as suggested previously by Christgen et al.  
254 (2015).

255

256 Overall, Figure 2 shows DDHS reactors are “efficient” at reducing both ARG and MGE  
257 levels. This is encouraging because DDHS systems use minimal energy compared to  
258 other available options for ARG and MGE removal (Bundy et al., 2017). For example,  
259 UV, advanced oxidation, and membrane bioreactor processes can effectively reduce  
260 ARGs (Wen et al., 2018; Zhang et al., 2016), but they use copious energy and too  
261 operationally complex for application where basic sanitation is lacking.



262

263 **Figure 2.** Total abundance of ARGs and MGEs detected in the raw wastewater and  
 264 DDHS reactor effluent samples conferring resistance to specific class of antibiotics. (A)  
 265 Absolute gene copy numbers per mL of wastewater; (B) Relative gene copy numbers  
 266 normalised to bacterial cell numbers derived from ambient 16S-rRNA gene abundances;  
 267 (C) Relative percentages of ARG abundances across samples. The line shows absolute  
 268 bacterial cell levels in the influent and effluents, which reflects eubacterial abundances  
 269 (error bars ~ small deviations concealed by marker). The blow-up insert shows subtle  
 270 differences among ARGs and MGEs in different DDHS reactor effluents. FCA =

271 fluoroquinolone, quinolone, florfenicol, chloramphenicol, and amphenicol ARGs;  
272 MLSB = Macrolide-Lincosamide-Streptogramin B ARGs.

273

### 274 **3.2.2. Relative ARG and MGE abundances**

275 Relative effluent ARG and MGE levels (normalised to bacterial cell abundances)  
276 display different removal patterns compared with absolute abundance data (Figure 2B).  
277 Relative ARG levels declined by ~70% in all four DDHS reactors, although dominant  
278 ARGs in effluents differed among bypass schemes. Specifically, relative effluent  
279 tetracycline and aminoglycoside ARG levels increased and MDR genes decreased with  
280 increased bypass, suggesting the aerobic top layer particularly enhances tetracycline and  
281 aminoglycoside ARG removal. In contrast, relative effluent MGE levels generally  
282 declined with increasing percent bypass, suggesting the anoxic layer may enhance MGE  
283 removal in DDHS systems.

284

285 DDHS reactors appear to be particularly effective at reducing medically important  $\beta$ -  
286 lactam and aminoglycoside ARGs. As examples, all DDHS configurations significantly  
287 removed ESBL- (e.g., *bla*<sub>CTX-M</sub>, *bla*<sub>SHV</sub>, *bla*<sub>TEM</sub>, *bla*<sub>SFO</sub>) and cephalosporin-resistance  
288 (e.g., *bla*<sub>cepa</sub> and *bla*<sub>AmpC</sub>) ARGs, which are often associated with Gram (-) enteric  
289 bacteria (Alouache et al., 2014; Blaak et al., 2015; Willemsen et al., 2015). Further, 2.0  
290 to 4.0 log reductions in culturable ESBL-producing *E.coli* and KESC (*Klebsiella*,  
291 *Enterobacter*, *Serratia* and *Citrobacter*) bacteria were observed in DDHS units (see  
292 Figure S2). Effluent ESBL-resistant isolate numbers increased with greater percent  
293 bypass and is consistent with ARG data.

294

295 DDHS reactors clearly reduce absolute ARG abundances from domestic wastewater.  
296 Estimated bacterial cell numbers in treated effluents showed 1.0 to 2.0 log reductions  
297 relative to influent levels (Figure 2B), with highest bacterial removals observed in R-  
298 S20. Further, bacterial removals parallel ARG removals, suggesting ARG reductions  
299 may be simply due to the removal of bacteria, which is greatest at intermediate bypass  
300 levels. This implies that ARG removal in DDHS systems may be primarily an  
301 ecological phenomenon, possibly including predation, which has been suggested  
302 previously for this type of reactor (Onodera et al., 2013). Conversely, TN removal  
303 increases with greater bypass, therefore an operational trade-off is needed to co-  
304 optimise TN and ARG removal for any application.

305

### 306 **3.3. Broader observations on ARG removal in bioreactors from DDHS systems**

307 Differences in ARG, MGE and bacterial removals across our DDHS systems permit  
308 some general observations about AMR removal in bioreactors. For example, data here  
309 suggest removal of common ARGs from wastewater is largely associated with  
310 removing bacteria, which in the case of DDHS systems, implies the top aerobic layer is  
311 particularly key to ARG removal. Previous work has shown aerobic processes may be  
312 better for ARG removal (Christgen et al., 2015), which data here suggest this may be  
313 due to greater bacteria removals. Specifically, as percent bypass is increased to a certain  
314 threshold (30% here), more influent bacteria (often anaerobes and facultative strains)  
315 “avoid” the aerobic treatment step, carrying and-or possibly exchanging ARGs in and  
316 through the lower anoxic layer. Therefore, although increasing percent bypass enhances  
317 denitrification, it allows bacteria to circumnavigate the aerobic layer. This is supported  
318 by the fact that relative ARG abundances are similar among effluents (Figure 2),  
319 suggesting absolute ARG in the effluents is mostly related to bacterial numbers.

320

321 In contrast, relative 'MDR' ARGs and also MGE abundances were lower in effluents  
322 when bypass is included (Figure 2B). The dominant ARG subclass in R-S0 effluent is  
323 MDR genes (~73%), whereas MDR only represents 44% of ARGs in R-S30 effluent  
324 (Figure 2C). Further, although absolute MGE levels increase with increasing bypass,  
325 relative MGE levels were highest in R-S0 and R-S10 with no or low bypass. This  
326 implies bacteria that survived both the aerobic and denitrifying layers tend to have  
327 greater genetic plasticity (i.e., higher MGEs per cell and potential for horizontal gene  
328 transfer, HGT), which may partially explain why such bacteria survive both redox  
329 environments.

330

331 An increase in MDR in aerobic processes has been seen previously (Czekalski et al.,  
332 2012; Pal et al., 2005; Yang et al., 2013), although a definitive explanation has not been  
333 provided. Higher MDR was previously explained by the presence of many micro-  
334 stressors in wastewater (e.g., metals, biocides etc.), which select for bacteria with  
335 multiple defence mechanisms (Christgen et al., 2015). However, our DDHS reactors  
336 had the same influent. Therefore, a better explanation is the change from an anoxic  
337 sewage environment to the aerobic treatment unit influences HGT, potentially selecting  
338 for MDR genotypes (Pal et al., 2005; Poole, 2012). This explanation is plausible  
339 because bacterial SOS stress responses cue HGT (Baharoglu et al., 2010) and a change  
340 in redox conditions would increase bacterial stress. However, a third explanation is that  
341 higher rates of HGT prevail under aerobic reactor conditions, possibly due to higher  
342 growth rates and greater bacterial densities. Suggesting aerobic units increase gross  
343 HGT is mildly controversial because others have found greater ARG HGT under  
344 anaerobic conditions (Rysz et al., 2013). However, data here imply the aerobic step in

345 DDHS systems is key to ARG removal, which is consistent with observations in other  
 346 studies (Farkas et al., 2016; Leverstein-van Hall et al., 2003; Mokracka et al., 2012;  
 347 Tennstedt et al., 2003; Zhang et al., 2009b).

348

349 **3.4. Persistent and unique ARG and MGE subtypes, and practical implications**

350 A Venn diagram of ARGs present in the influent and effluents is provided as Figure 3.

351 It shows 10 “persistent” ARGs (i.e., not removed by any configuration) across all

352 reactors and also unique ARGs among different effluents (see Table S4 for specific

353 ARGs). Overall, effluent from R-S0 had the highest number of unique ARGs (10),

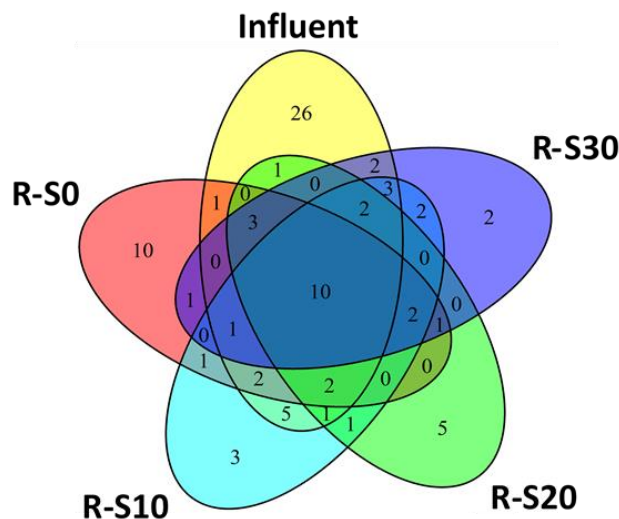
354 whereas R-S30 effluents had lowest number of unique ARG numbers (2), although R-

355 S30 also had the highest absolute bacterial and ARG abundances. ARGs in the central

356 overlap were persistent in all effluents (see Table S3), including *tetQ*, *tetM*, *tetX*,

357 *bl2d\_oxa10*, and *qacEdelta1*; ARGs often associated with acquired resistance (van

358 Hoek et al., 2011).



359

360 **Figure 3.** Venn diagram showing overlap of ARGs among influent and effluent samples

361 from different DDHS configurations. Subsets represent number of genes detected in the

362 wastewater influent (59 ARGs); R-S0 (35 ARGs); R-S10 (35 ARGs); R-S20 (28 ARGs)

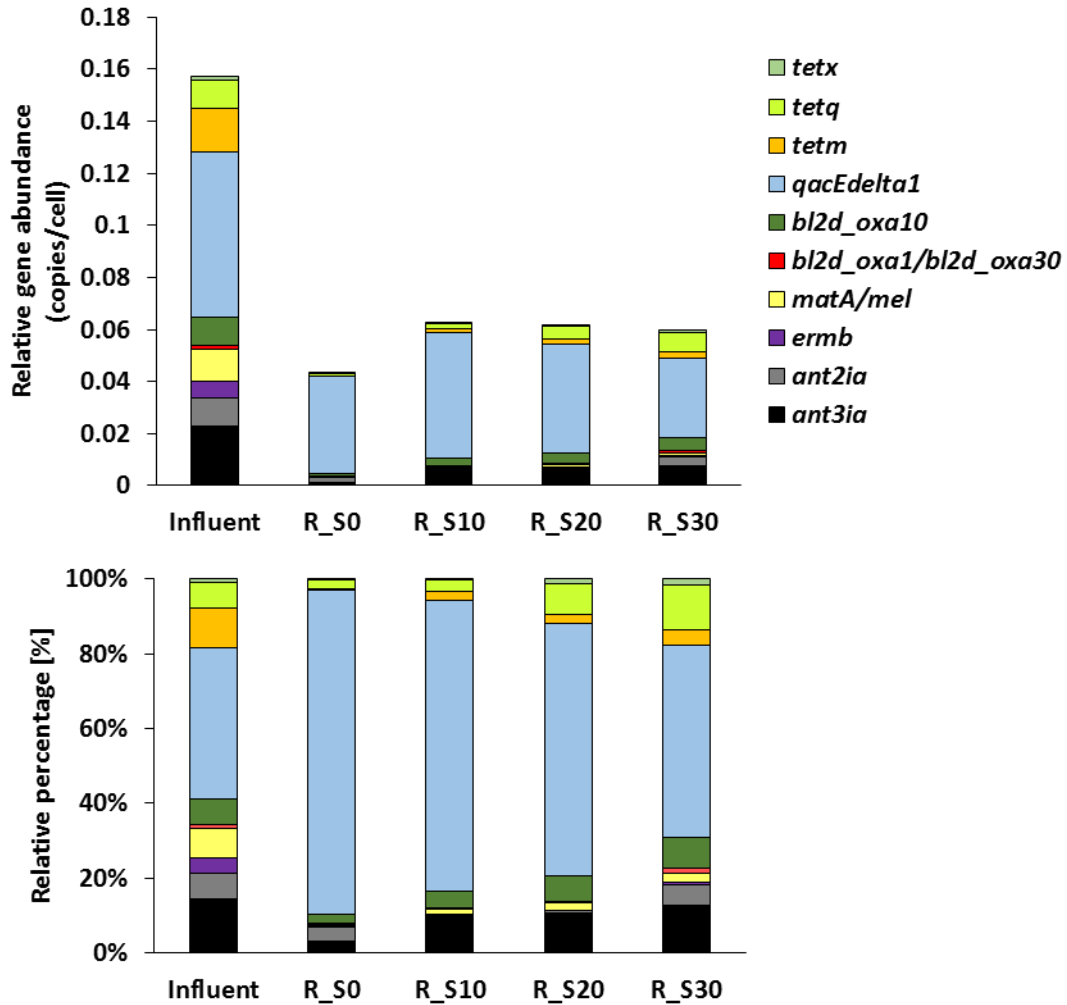
363 and R-S30 (30 ARGs). The central overlap represents the number of persistent ARGs.



364

365 All persistent ARGs are summarised in Figure 4 and statistical associations with  
366 persistent MGEs are provided in Table S5. First, persistence appears strongly associated  
367 with MDR genes, especially in no or low bypass reactors. However, if one looks at the  
368 implied MDR signal, only one ARG is apparent, *qacEdelta1*, which is closely  
369 associated with integron cassettes (Partridge et al., 2009) and only correlates with *int1*  
370 and *Cint1* (Table S5). In data here, more of the persistent ARGs statistically correlate  
371 with *tp614* (especially tetracyclines and ESBL ARGs), which codes for a transposable  
372 element often linked to carbapenem resistance (Soki et al., 2006). This does not mean  
373 *tp614* is carrying these ARGs, but implies integron genes are not directly associated  
374 with the most persistent ARGs in DDHS effluents.

375



376

377 **Figure 4.** Persistent ARGs not removed in any DDHS reactor configuration. Relative  
 378 abundances of persistent ARGs in the influent and effluents of each reactor (top panel;  
 379 ARGs noted in the legend), and corresponding relative percentages of ARGs in reactor  
 380 influent and effluent based on proportion of total ARG copy numbers (bottom panel).

381

#### 382 4. Conclusions

383 DDHS and other sponge reactors are an attractive option for small-scale wastewater  
 384 treatment. Kobayashi et al. reported sponge systems effectively remove pathogenic  
 385 viruses (1.5 to 3.7 log reduction for aichivirus, novovirus and enterovirus) (Kobayashi  
 386 et al., 2017), which complements results here on AMR removal. In particular, DDHS  
 387 systems can reduce both TN and AMR from domestic wastewater (contrary to other

388 sponge designs) and are suitable for small-scale applications due to low energy and  
389 maintenance needs.

390

391 Based on high ARG removal levels, the potential for TN removal, and low energy  
392 demands, DDHS systems show great promise at reducing environmental and health  
393 impacts of wastewater discharge on local scales. As such, they should be considered in  
394 locations where centralised treatment does not exist or would be costly, although co-  
395 optimization is needed to satisfy local priorities relative to ARG versus TN removal.

396

### 397 **Acknowledgement**

398 Authors acknowledge funding support by an UK Engineering and Physical Science  
399 Research Council Impact Acceleration Award, entitled “‘Demonstrating Low-energy  
400 Technologies for Decentralised Waste Treatment around the World” (EP/K503885/1);  
401 AstraZeneca Global Environment; and the National Natural Science Foundation of  
402 China (Award 21210008).

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